

Low-Energy Inland Brackish Water Desalination

WRRC Water Webinars 104(b) Student Research Presented By: Arianna Tariqi



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United Nations Sustainable Development Goals



SAFE AND AFFORDABLE DRINKING WATER

By 2030, achieve universal and equitable access to safe and affordable drinking water for all.



To meet the 2030 target year, the pace of progress will need to accelerate... **6X for global coverage of Drinking Water**

INCREASE WATER-USE EFFICIENCY AND ENSURE FRESHWATER SUPPLIES

By 2030, substantially increase water-use efficiency across all sectors and ensure sustainable withdrawals and supply of freshwater to address water scarcity and substantially reduce the number of people suffering from water scarcity.

Water Shortages

California's drought stripes



Arizona Limits Construction Around Phoenix as Its Water Supply Dwindles

In what could be a glimpse of the future as climate change batters the West, officials ruled there's not enough groundwater for projects already approved.



Lake Mead



Updated November 25th 2023

Inland Desalination



ntroduction



The world's drinking water supply is at risk and desalination plants are set to make more saltwater potable. But to make the process sustainable and affordable, new and improved technologies need to be further developed

ntroduction





NF90 NF270

Yuma Desalting Facility



Methods

Working with ESU unit

- 2:1 array
- RO feed water is pretreated main outlet drain extension (MODE) surface water available at the YDP (2000 mg/L TDS). We used BW30-2540, NF90-2540 and NF270-2540 membranes



Hypothesis

Including Nanofiltration in the industry baseline desalination treatment train at different stages or as a pre/post treatment to reverse osmosis (RO) can aid the desalination process by improving RO performance and overall lowering energy requirements of the desalination process.

Objectives

1. Assess the best hybrid configuration to increase membrane lifetime, further concentrate brine, decrease specific energy consumption (SEC), and increase water quality.

2. Identify a modeling strategy that can effectively compare the tradeoffs between rejection, water flux, cost, and system energetics of NF-RO and RO-NF compared to conventional RO.



Reverse Osmosis System Configuration





Iethods

Challenges

- -High energy consumption
- -High scaling potential **Additional**
 - -Large volumes of brine as a
 - byproduct
 - -High cost depending on TDS





Reverse Osmosis System Configuration Integrating NF90 Membrane



NF90

 $Q_{p2,C_{p2}}$

 $Q_{r_2,C_{r_2}}$

Iethods





One Stage Reverse Osmosis System Configuration Pre/Post Treating using NF270



Jethods



Equations for Performance Metrics





Jethods



Recovery

Product Flow * 100% Feed Flow



Product/Permeate



System Modeling





0.1 Million Gallons / Day

Scaling up the Units 10 X







1 Million Gallons / Day







Iethods

System Model Using WAVE

Configured a larger pilot system on WAVE that simulates a 1MGD plant

✤ WAVE has inputs such as

- Feed flows
- Feed water quality -
- Recovery
- Membrane type
- Stages
- Membrane elements

Feed water quality:

Table 1 Pretreated MOD

Ion

Barium Calcium Chloride Magnesium Nitrate as N Potassium Sodium Strontium Sulfate Conductivity pН **Total Alkalinity** TDS (mg/L)



E Feed Water Con	nposition							
Concentration								
	(mg/L)							
	0.012							
	85.8							
	541.5							
	50.0							
	6.6							
	6.9							
	528.8							
	1.26							
	764.9							
	3,192							
	6.12							
	5.8							
	2,015							





Components

High pressure pump +Booster pump + Membrane modules + Waste Disposal

Annual Fixed O&M

Annual O&M cost divided by the total permeate water produced in one year





Pilot System Results - Salt Rejections



Results

✤ RO-NF90 and NF90-RO have lower rejections of monovalent ions compared to the baseline RO-RO and NF270 configurations ◆ NF270-RO has the highest rejections greater than 99% for monovalent and divalent **1011**S





Pilot System Results– Recovery and SEC



* Comparing the function of the RO when pre/post-treating

esults

40Reco

2 ~50% lower SEC of the RO element when pre/post-treating while increasing the recovery of the system by $\sim 25\%$

 \therefore NF90-RO is ~60% less than the baseline RO-RO configuration





esults

Modeled Results- SEC and Recovery



* Comparing the function of the RO when pre/post-treating



Closer to typical SEC values of BW desalination



Follows the same trend as the pilot system





Modeled Results– Recovery and SEC



* Comparing the function of the RO when pre/post-treating

Results



Further concentrating the brine using the NF270, the recovery increases while the SEC decreases





Results

Modeled Results- Cost of Variable O&M



When pre-treating, the variable operating cost of RO decreases by 60%

Post-Treating decreases cost buy 43%





Results

Modeled Results– Cost



 Adding the additional cost of treatment using the NF270 membranes drastically increases the NF270-RO cost

RO-NF270 cost remains
~40% lower than RO RO



Conclusions- Tradeoffs



Results



Next Steps-Analysis of Scaling of the systems

Done

 Increased concentration of the feed stream to speed up scaling process
Analyze flows and pressure changes

Working on

- Membrane Autopsies
- Analysis of the membranes (SEM, contact angle, zeta potential)









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WATER RESOURCES RESEARCH CENTER

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Thank you Questions?

System parameters- Salt Rejections

1st stage

Results

RO Salt Rejection Heatmap

		NESTOR O	DONICOTO	
	99.7%	85.7%	91,5%	
	100:0%	98.2%	11.4%	- 0.2
	100.0%	99.9%	12.3%	- 0.4
	99,0%	98.6%	31.6%	- 0.6
	99.1%	99.0%	35.9%	- 0.8
e i	98.9%	99.3%	2.9%	- 1.0

2nd stage

- Chloride
- Sodium
- Magnesium
- Calcium
- Sulfate

Feed of the overall configuration
versus the feed entering the 2nd stage RO membranes
Mainly consists of monovalent ions

- Chloride
- Sodium
- Magnesium
- Calcium
- Sulfate

Typical Feed concentrations of the configurations and the 2nd stage permeate that will be entering back into the feed. Higher Monovalent ions, less divalent

Reduced Sulfate

concentrations

HE UNIVERSITY **OF ARIZONA**

	reeu		Feed			Feed	_		Feed	_		Feed	-			
			recu	5			5			-			_		reeu	
NH4+	0.00	NUL 4	0.00	+	NH₄+	0.00		NH4+	0.00		NH4 ⁺	0.00	_			┢
K+	6.93	NH4 ⁺	0.00	-	K+	8.79	:	K+	9.08		К+	9.21		NH4+	0.00	-
Na+	528.6	K+	8.15	_	Na+	674.9		Na+	698.2		Na+	708.7		K+	9.27	
Mg+2	50.26	Na+	624.2	_	Ma+2	53.18		Ma+2	54.08		Mg+2	54.47		Na+	713.4	
Ca+2	85.74	Mg+2	51.18		Ca+2	02.04			02.79		Ca+2	94.52	_	Mg+2	54.63	
Sr+2	1 25	Ca+2	88.22		Cu la	1.00	-	Care	93.76		Sr+2	1.37		Ca+2	94.84	
D- + 0	0.01	Sr+2	1.28		Sr+2	1.33	_	Sr+2	1.36		D-+0	0.00		Sr+2	1.37	
Ba≁∠	0.01	Ba+2	0.01		Ba+2	0.01		Ba+2	0.02		Ba+7	0.02	_	D 2+2	0.02	
03-2	0.00		0.01	-	CO3-5	0.00		CO3-5	0.00		CO3-5	0.00	_	Dd	0.02	ŀ.
CO3-	7.08	CO3-2	0.00	-	HCO3⁻	8.97	—	HCO3⁻	9.08		HCO3-	9.07		CO3-5	0.00	_
NO3-	6.64	HCO3-	8.75		NO ₂ -	10.92		NO ₂ -	11 50		NO3-	11.92		HCO3⁻	9.07	
F-	2.60	NO3⁻	9.53			4.00	-	INOS	11.39		F-	4.37	_	NO₃⁻	12.08	
	544.0	F-	3.63		F-	4.08		F-	4.28				_	F-	4.41	<u> </u>
а-	541.9	CI-	757.3	-	CI-	851.3	:	CI-	893.1		a-	911.7	_	cl-	010.0	F.
Br-1	0.00			-	Br-1	2.20		Br-1	2.68		Br-1	2.55		- u	919.9	-
04-2	765.5	Br-1	2.97	-	SO4-2	671.7	—	S04-2	670.7		SO4-2	670.4		Br-1	2.62	Ļ.
04-3	2.60	SO4-2	678.2		PO4-3	1.60		PO₄-3	1.17		PO4-3	1.42		SO4-2	670.3	
SiO2	8.91	PO4-3	0.00		SiO2	13.60	-	SiOn	14.42		SiO2	14.86		PO4-3	1.35	
Boron	0.80	SiO2	11.98		Boron	0.90		5102	14.45		Boron	0.90	_	SiO2	15.09	
	5.00	Boron	0.87		DOLOU	0.69		Boron	0.90			5.55		Boron	0.90	
CO2 5.88	.88	8		+	- CO-	5 02		CO2	5.88		CO2	5.90				

